

# Biassing a Diode Laser at the Self-Mixing Crossover Improves Immunity to Backreflection

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**Abstract:** The adverse effects of back-reflected waves on a diode laser used as a transmitter can be substantially mitigated if the current biasing is set at a specific value, the self-mixing crossover which can be found by a simple setup. A de-sensitization of the reflection effects by a factor of 25 dB has been observed.

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## 1. Introduction

As it is well known, retro-reflected waves affect the operation of a single-mode laser used as a transmitter, impairing both line width and phase noise. Insertion of an optical isolator is mandatory between the source and the line. On the other hand, reflected waves are used to advantage in the self-mixing interferometer (SMI). In the SMI, light from a single-mode laser diode is focused on the remote target, and a fraction of the back-scattered light re-enters the laser cavity, where it is coherently mixed with the lasing field. This induces a modulation of the emitted power in form of an interferometer signal with the phase information of path length traveled by the field from the laser cavity to the target and back [1,2]. The signal is detected by the monitor photodiode usually provided in the laser package. Of course, the difference between the two cases above is that back reflection is not under a good control for the transmitter laser, whereas it is a slow-varying and coming from a well defined distance in the latter case.

Recently, we have carried out an analysis [3] to compare the different signals available in a SMI (Fig.1):  $S_1$  exiting from rear-mirror,  $S_2$  from the front mirror on the same side of the remote target, and  $V_{ak}$  across the junction. Analyzing these signals, we find that the front mirror  $S_2$  changes from in-phase to a phase-opposition respect to  $S_1$  and  $V_{ak}$ , as bias current is increased. This is because the field reflected at the front mirror (folded arrow in Fig.1) is added to the field leaving the laser whereas it is missing from the rear-mirror. Denoting with  $m_1 = \Delta S_1/S_1$  the modulation index of the self-mixing signal  $\Delta S_1$  superposed on a dc component  $S_1$ , and similarly for  $m_2 = \Delta S_2/S_2$ , the analysis according to the scheme of Fig.1 provides the following results [3]:

$$m_1 = (-T_1/\sqrt{R_1}) \sqrt{A} \cos 2ks [(2\gamma L \ln R_1 R_2) - 1] \quad (1)$$

$$m_2 = (-T_1/\sqrt{R_1}) \sqrt{A} \cos 2ks [(2\gamma L \ln R_1 R_2) - 1 - R_1/T_1] \quad (2)$$

Here  $T$ ,  $R$  are the (power) transmission and reflection of mirrors,  $A$  is the attenuation in propagation up to target at distance  $s$  and back, and  $2\gamma L$  is the gain per pass of the laser. Term  $-R_1/T_1$  at the right hand side of Eq.2 is the contribution reflected from the front output mirror. The minus sign is due to a double passage of this contribution in reflection respect to the other in transmission, resulting in a cumulative  $2(\pi/2) = \pi$  phase difference.

Examples of waveforms  $\Delta S_1$  and  $\Delta S_2$  measured with the self-mixing interferometer are shown in Figs. 2 and 3. In the setup, we used an 825-nm laser diode from Hitachi (ML8325) and a collimator lens to focus the spot on the target, a piece of white paper glued on a loudspeaker. The loudspeaker was driven by a sine wave at audio frequency, with a few wavelengths of amplitude swing. In addition, writing the gain per unit length as [3]:

$$\gamma = A I_{bias} - B \quad (3)$$

where  $I_{bias}$  is the current fed to the laser diode, and  $A$ ,  $B$  are constants, we can express Eqs.1 and 2 in term of the bias  $I_{bias}$  and be able to calculate the ratio  $m_1/m_2$  of modulation index, as plotted in the diagram of Fig.4. Here, the experimental points come from measurements of waveforms like those in Fig.3, at different currents.

From the above discussion, it is clear that the disturbance due to reflected wave is ideally canceled out in the front output  $S_2$  at the crossover point  $I_{bias} = I_{CO}$ . To evaluate in a practical case the cancellation, we may define a back-reflection suppression ratio BSR as the reduction (in dB) of the spurious components added to the signal spectrum. If the spurious component of  $S_1$  is taken as the reference, then the suppression ratio easily follows as  $BSR = 10 \log_{10}[m_1/m_2]$ . In Fig.5 we plot the experimental frequency spectrum measured at crossover and at high current (where  $m_1/m_2 \approx 1.2$ ). The peak corresponding to the fundamental frequency content of the self-mixing signal

(waveform of Fig.2) is reduced of about 25 dB by working at a bias near the crossover.

**References**

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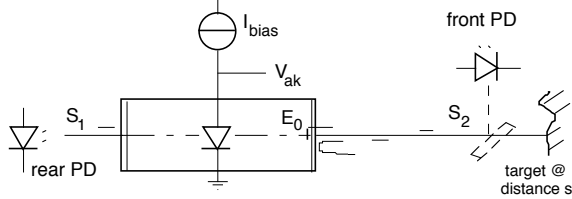


Fig. 1. Signals available in a self-mixing interferometer:  $S_1$  is taken at the rear-mirror output (usually by the monitor photodiode);  $S_2$  is the output from the front mirror, and  $V_{ak}$  is the voltage across the laser diode junction. Analyzing these signals one can find that  $S_2$  has a crossover (vanishes) at a certain bias current, whereas  $S_1$  and  $V_{ak}$  increase monotonically with  $I_{bias}$ .

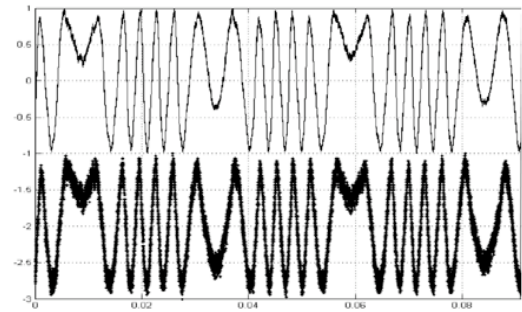


Fig. 2. Rear (top) and front (bottom) output signals,  $S_1$  and  $S_2$ , taken moderate bias  $I_{bias}=50$  mA where they are in-phase. The target is a loudspeaker driven at audio frequency with a sine wave at  $\approx 4 \mu\text{m}$  peak-to-peak amplitude.

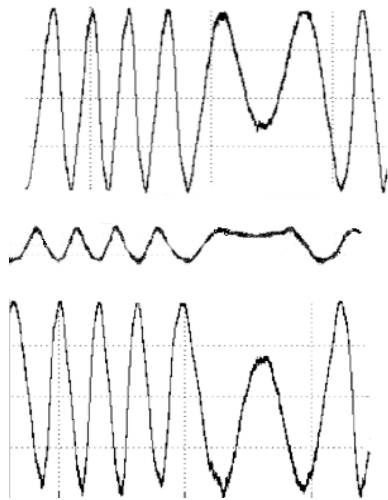


Fig. 3. Self-mix signal  $S_2$  at different bias currents. Top:  $I_{bias}=50$  mA, moderately above threshold; middle:  $I_{bias}=58$  mA, about the crossover; bottom: well above threshold, at  $I_{bias}=80$  mA where the self-mixing signal  $S_2$  has changed polarity respect to  $S_1$ .

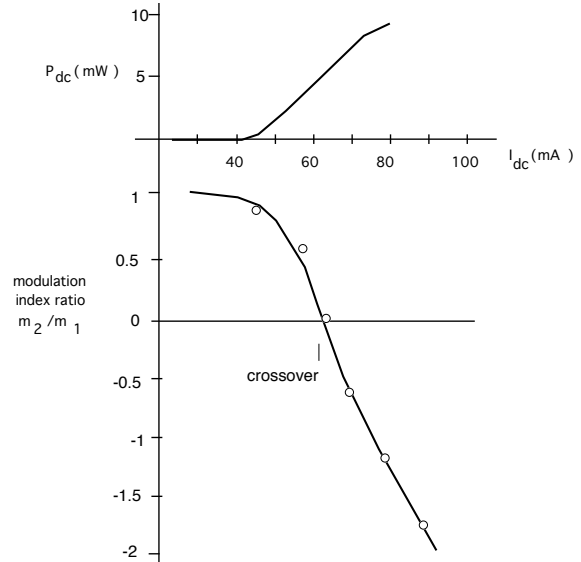


Fig. 4. Power-current diagram (top) and the ratio of modulation index  $m_2/m_1$  versus bias current. Threshold is at 45 mA and the crossover of  $S_2$  signal at a bias of about  $I_{bias}=63$  mA. Dots are experimental points.

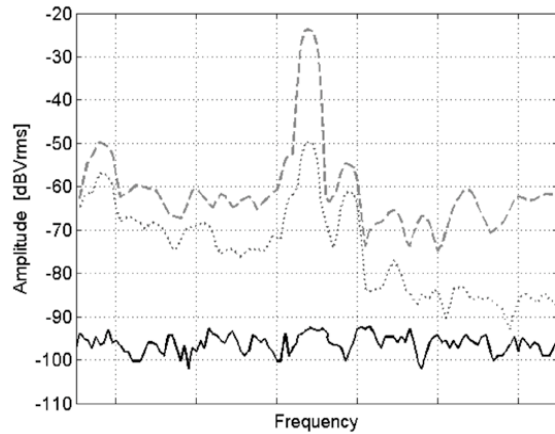


Fig. 5 The frequency spectrum of signal  $S_2$  for  $I_{bias}=80$  mA (at which  $m_2/m_1=-1.2$ ), top trace, and at  $I_{bias}=I_{CO}=60$  mA (at which  $m_2/m_1\approx 0$ ), middle trace; noise floor is the bottom trace. No optical isolator is used. The peak corresponds to the fundamental frequency contained in the signals of Fig.2. The disturbance is reduced, comparing the top and middle traces, of a factor  $BSR \approx 25$  dB.